

STEFAN PROBLEMS AND KINETICALLY CONSTRAINED LATTICE GASES

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Structure of the talk

1 **Intro: hydrodynamics and KCLG's**

2 **The Facilitated exclusion process**

- Hydrodynamics for the FEP
- Equilibrium distributions
- Estimation of the transience time

3 **Higher dimension and boundary interactions**

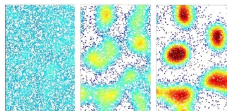
- CLG_2 and FEP_2
- Diffusion coefficient and reservoirs

4 **Comments and (some) open problems**

STATISTICAL PHYSICS AND HYDRODYNAMIC LIMITS

Linking micro/macro levels of description for a variety of physical systems to prove phase transition phenomena for out of equilibrium systems. Some examples :

- ▷ **Active matter** models : spontaneous condensation (MIPS) and onset of collective motion (travelling waves).



- ▷ **Non-equilibrium** models, e.g. boundary-driven systems.

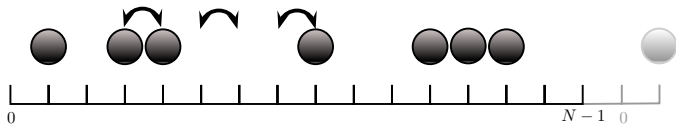


- ▷ **Kinetically constrained lattice gases** to model the liquid-solid phase transition.



AN ELEMENTARY EXAMPLE : SYMMETRIC SIMPLE EXCLUSION PROCESS (SSEP)

- Bulk $\Lambda_N = \{0, \dots, N - 1\}$ with periodic boundary conditions.
- Configuration $\eta \in \Omega_N := \{0, 1\}^{\Lambda_N}$, with $\eta_x = 1$ for an occupied site, $\eta_x = 0$ for an empty site.
- *Stirring dynamics*: two neighboring sites are exchanged at rate 1.



Assuming that the initial configuration $\eta(0)$ is “close” to a macroscopic profile $\rho_0 : [0, 1) \rightarrow [0, 1]$, the macroscopic evolution of the system is ruled by the heat equation

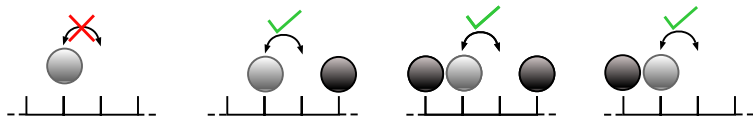
$$\begin{cases} \partial_t \rho = \partial_{uu} \rho \\ \rho(0, \cdot) = \rho_0 \end{cases},$$

where ρ is the density field, “ $\rho(t, u) = \mathbb{E}(\eta_{uN}(tN^2))$ ”.

KINETICALLY CONSTRAINED LATTICE GASES

Question: What happens if a kinetic constraint is added to the dynamics ?

Example: [Gonçalves, Landim, Toninelli '08]:



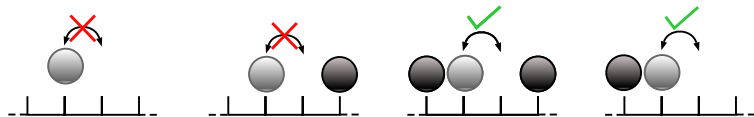
With the right jump rates, the hydrodynamic behavior for this macroscopic system is ruled by the *porous medium equation*

$$\begin{cases} \partial_t \rho = \partial_{uu} \rho^2 \\ \rho(0, \cdot) = \rho_0 \end{cases} .$$

- ▶ Bernoulli product measures are reversible for this process.
- ▶ *Mobile cluster*: two consecutive particles can move around the system and locally mix the system. \mapsto local ergodicity.

FACILITATED EXCLUSION PROCESS (FEP)

Stronger kinetic constraint than in [Gonçalves, Landim, Toninelli '08]: A particle can jump to a neighbor site iff its other neighbor is occupied.



Markov generator:

$$\mathcal{L}_N f(\eta) = \sum_{x \in \Lambda_N} c_{x,x+1}(\eta) \{f(\eta^{x,x+1}) - f(\eta)\},$$

with

$$c_{x,x+1}(\eta) = \eta_{x-1}\eta_x(1 - \eta_{x+1}) + \eta_{x+2}\eta_{x+1}(1 - \eta_x),$$

and $\eta^{x,x+1}$ is the configuration where sites x and $x+1$ have been exchanged.

- ▶ Bernoulli product measures are not stationary.
- ▶ No longer a *mobile cluster* to mix the configuration.

HYDRODYNAMIC LIMIT FOR THE FEP

We start the process from a product measure μ_N “fitting” a macroscopic profile $\rho_0 : [0, 1] \rightarrow [0, 1]$, i.e. $\mu_N(\eta_x = 1) = \rho_0(x/N)$.

Theorem (Blondel, E', Simon, Sasada 2018 & BES 2021)

Consider the process $\eta(t)$ started from the measure μ_N , and driven by $N^2 \mathcal{L}_N$. Given an initial profile ρ_0 , we have for any test function H

$$\frac{1}{N} \sum_{x \in \Lambda_N} H(x/N) \eta_x(t) \xrightarrow[N \rightarrow \infty]{\mathbb{P}} \int_{[0,1]} H(u) \rho(t, u) du$$

where ρ is solution to the Stefan problem $\rho(0, u) = \rho_0(u)$ and

$$\boxed{\rho_0 > 1/2}$$

$$\boxed{\rho_0 \in [0, 1]}$$

$$\partial_t \rho = \partial_{uu} \left\{ \frac{2\rho - 1}{\rho} \right\}$$

$$\partial_t \rho = \partial_{uu} \left\{ \frac{2\rho - 1}{\rho} \mathbf{1}_{\{\rho \geq 1/2\}} \right\}.$$

TYPES OF CONFIGURATIONS

Define $\Omega_N^k = \{\eta \in \Omega_N, \sum \eta_x = k\}$, there are four types of configurations:

- If $k \leq N/2$, $\Omega_N^k = F_N^k \cup TB_N^k$:

Frozen configurations

$$F_N^k = \{\eta \in \Omega_N^k \mid \eta_x \eta_{x+1} \equiv 0\}$$



Transient Bad configurations

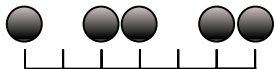
$$TB_N^k = \{\eta \in \Omega_N^k \mid \eta_x \eta_{x+1} \neq 0\}.$$



- If $k \geq N/2$, $\Omega_N^k = E_N^k \cup TG_N^k$:

Ergodic configurations

$$E_N^k = \{\eta \in \Omega_N^k \mid (1-\eta_x)(1-\eta_{x+1}) \equiv 0\}$$



Transient Good configurations

$$TG_N^k = \{\eta \in \Omega_N^k \mid (1-\eta_x)(1-\eta_{x+1}) \neq 0\}$$



EQUILIBRIUM DISTRIBUTIONS

For $k \geq N/2$, the uniform distribution π_N^k on E_N^k satisfies *detailed balance*, and is therefore a reversible measure for the process on E_N^k , so that one only needs to compute $|E_N^k|$.

To do so, two possibilities for the first site of the configuration:

- If occupied, we have $N - k$ empty sites, to be placed in k interstices between particles.
- If empty, it is surrounded by particles, and we have $N - k - 1$ empty sites, to be placed in $k - 1$ interstices between particles.

$$|E_N^k| = \binom{k}{N-k} + \binom{k-1}{N-k-1}$$

GRAND CANONICAL MEASURES

With similar combinatorial arguments, given a configuration σ on a box $\{1, \dots, \ell\}$, one can compute

$$\pi_N^k(\eta_{\{1, \dots, \ell\}} = \sigma) = \frac{|\{\eta \in E_N^k, \eta_{\{1, \dots, \ell\}} = \sigma\}|}{|E_N^k|}.$$

As $N \rightarrow \infty$ and $k/N \rightarrow \rho > 1/2$,

$$\pi_N^k(\eta_{\{1, \dots, \ell\}} = \sigma) \xrightarrow{N \rightarrow \infty} \pi_\rho(\eta_{\{1, \dots, \ell\}} = \sigma)$$

defines the grand canonical measure π_ρ on the set of infinite ergodic configurations.

- ▷ π_ρ is supported on the infinite ergodic component.
- ▷ π_ρ is a Bernoulli product measure conditioned to having isolated empty sites (ergodic component)
- ▷ π_ρ exhibits **long-range correlations** as $\rho \searrow 1/2$.

ENTROPY TOOLS AND EQUILIBRIUM DISTRIBUTIONS

The most classical techniques for hydrodynamic limits are based on **entropy bounds** between the measure μ_t^N of the process at time t and its reference measures π_α , namely

- ▷ Guo, Papanicolaou and Varadhan's **entropy method**,

$$H(\mu_t^N \mid \pi_\alpha) \leq CN,$$

- ▷ Yau's **relative entropy method**

$$H(\mu_t^N \mid \pi_{\rho_t}) = o(N).$$

Supercritical case, in the transient regime, μ_t^N is not supported on ergodic configurations, whereas the grand canonical measures π_ρ are \Rightarrow entropy estimate fails. In particular, we need to prove that the ergodic component is reached quicker than the diffusive timescale $\tau = O(N^2)$.

General case, no hope of using the entropy method : no reference measures because the two phase's stationary states have **disjoint supports**.

ESTIMATION OF THE TRANSIENCE TIME

Theorem (Thermalization of the supercritical phase, BESS18)

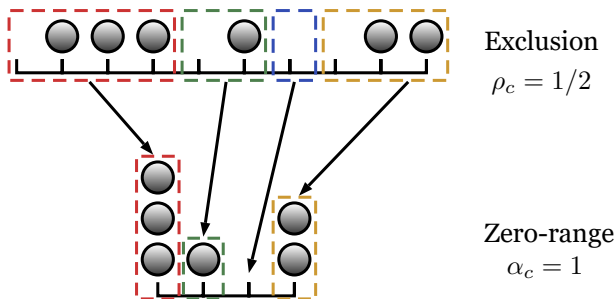
Assume that $\rho_0 > 1/2$. There exists α such that, letting $t_N = (\log N)^\alpha / N^2$ and k_0 the initial number of particles in the configuration,

$$\lim_{N \rightarrow \infty} \mathbb{P}(\eta(t_N) \notin E_N^{k_0}) = 0.$$

Theorem (Thermalization in a general case, BES21)

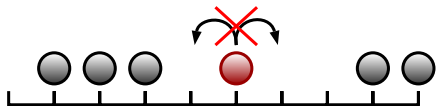
- ▷ The ergodic and frozen phases thermalize w.h.p in a time of order $t_N = (\log N)^\alpha / N^2$.
- ▷ A critical interface a , assuming $\partial_u \rho_0(a) \neq 0$ thermalizes w.h.p in a time of order $t_N = N^{-\varepsilon}$.
- ▷ Otherwise, (i.e. if $\partial_u \rho_0(a) = 0$), the “thermalization time” t_N is $O(1)$.

TRANSIENCE TIME : MAPPING WITH A ZR PROCESS



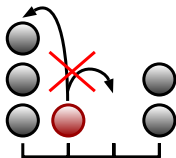
- ▷ This zero-range process is **attractive**.
- ▷ To understand the **supercritical** transience time, one needs to estimate the time the zero-range takes to **fill all empty sites** in the supercritical region.
- ▷ To understand the **subcritical** transience time, one needs to estimate the time the zero-range takes for all particles to **fall in an empty site**.

TRANSIENCE TIME : MAPPING WITH A ZR PROCESS



Exclusion

$$\rho_c = 1/2$$



Zero-range

$$\alpha_c = 1$$

- ▷ This zero-range process is **attractive**.
- ▷ To understand the **supercritical** transience time, one need to estimate the time the zero-range takes to **fill all empty sites** in the supercritical region.
- ▷ To understand the **subcritical** transience time, one needs to estimate the time the zero-range takes for all particles to **fall in an empty site**.

Theorem (Blondel, E', Simon, Sasada 2018 & BES 2021)

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where ρ is solution to the Stefan problem $\rho(0, u) = \rho_0(u)$ and

$$\boxed{\rho_0 > 1/2}$$

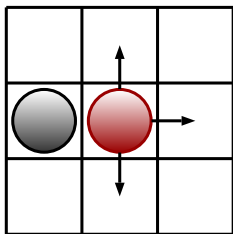
$$\boxed{\rho_0 \in [0, 1]}$$

$$\partial_t \rho = \partial_{uu} \left\{ \frac{2\rho - 1}{\rho} \right\}$$

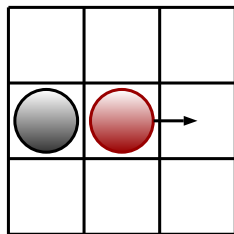
$$\partial_t \rho = \partial_{uu} \left\{ \frac{2\rho - 1}{\rho} \mathbf{1}_{\{\rho \geq 1/2\}} \right\}.$$

- ▶ Supercritical case $\rho_0 > 1/2$: thermalization+ properties (*decorrelation, equivalence of ensembles*) of $\pi_\rho, \pi_N^k \implies$ Hydrodynamic Limit (Entropy Method, Guo, Papanicolaou, Varadhan, '88)
- ▶ General case $\rho_0 \in [0, 1]$: proved adapting a result by Funaki '99. Requires some De Finetti type result on the decomposition of translation invariant stationary measures for the process.

ANALOGOUS MODELS IN DIMENSION D=2



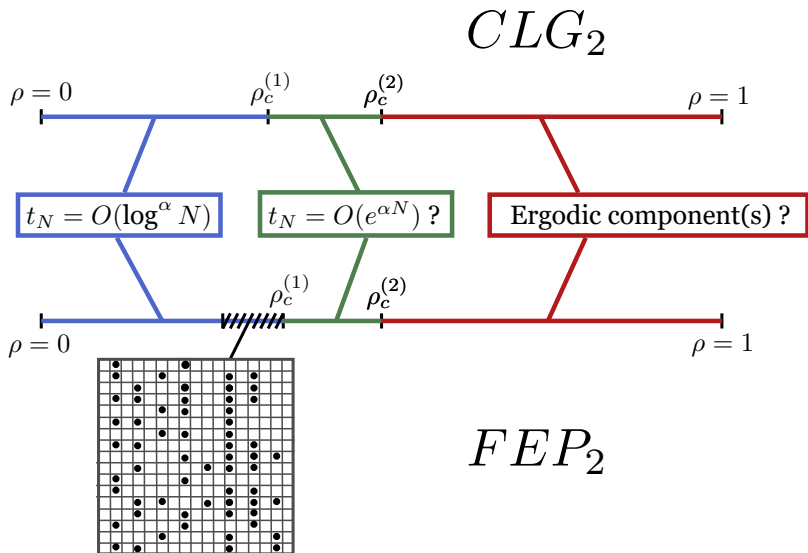
CLG_2



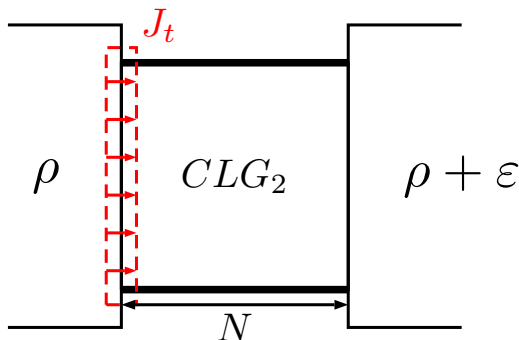
FEP_2

- ▷ In two dimensions, several critical density threshold : threshold for **ergodicity**, threshold for **subdiffusive transience**.
- ▷ All tools developed for dimension 1 fail, zero-range mapping no longer available : hydrodynamic behavior out of reach.
- ▷ for FEP_2 , another critical density with onset of quasi-1-dimensional behavior for $\rho \leq 1/4$

CRITICAL DENSITIES FOR CLG_2 AND FEP_2



DIFFUSION COEFFICIENT AND RESERVOIR INTERACTION



For the diffusion coefficient $D(\rho)$ of the $2d$ system, with “hydrodynamics”

$$\partial_t \rho = \nabla \cdot D(\rho) \nabla \rho,$$

the following gives a concrete computation scheme;

- ▷ System in contact with two reservoirs, left density ρ , right density $\rho + \varepsilon$
- ▷ Stationary regime: left boundary total current $J_t \simeq -NtD(\rho)\nabla_{0,1}\rho$.

$$\implies D(\rho) = - \lim_{t \rightarrow \infty} \lim_{\varepsilon \rightarrow 0} \frac{J_t}{t\varepsilon}.$$

RESERVOIR INTERACTION AND HYDRODYNAMICS

- ▶ When a particle system is affected by a non-conservative reservoir dynamics with equilibrium density α , The hydrodynamic will typically exhibit **Dirichlet boundary conditions** with the same value α as the reservoir.
- ▶ For exclusion dynamics, a typical reservoir dynamics consists in filling an empty site at rate α and emptying an occupied site at rate $1 - \alpha$.
- ▶ In the case of kinetically constrained models, the interplay between boundary dynamics and bulk dynamics is less straightforward because of the **frozen phase**.
- ▶ In the frozen phase, there is no diffusion until the system locally reaches the critical density. In particular, a subcritical reservoir dynamics $\alpha < \rho_c$ will, microscopically enforce a **supercritical effective density** $\alpha_{\text{eff}} > \rho_c$.

DIFFUSION COEFFICIENT AND RESERVOIR INTERACTION

- ▷ It seems like the diffusion coefficient is continuous on $\rho \in [0, 1]$.
- ▷ The definition of the diffusion coefficient itself is problematic, since there is no diffusion under density $\rho_c \simeq 1/3$
- ▷ Even subcritical reservoirs enforce an **effective supercritical density**, and this density is larger than ρ_c
- ▷ Delicate interpretation of this quantity in the subcritical regime.

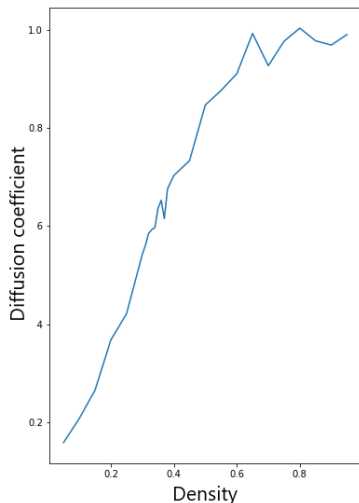


Figure: Simulation by A. Roget

COMMENTS AND OPEN PROBLEMS

- ▷ Hydrodynamic limit result in **one dimension with subcritical reservoirs** ?
- ▷ Starting from an empty configuration with subcritical reservoir, **front progression** on a timescale $t = O(N^3)$?
- ▷ Explicit expression and characterization of **critical densities** 2 dimensions ? Can we uncover the **structure of the ergodic configurations** ?
- ▷ Can we tackle **other kinetic constraints**, in dimension 1 ? Is there an analogous separation in ergodic/frozen phases ?